

Optical Remote Sensing with Differential Absorption Lidar (DIAL)

Part 1: Theory

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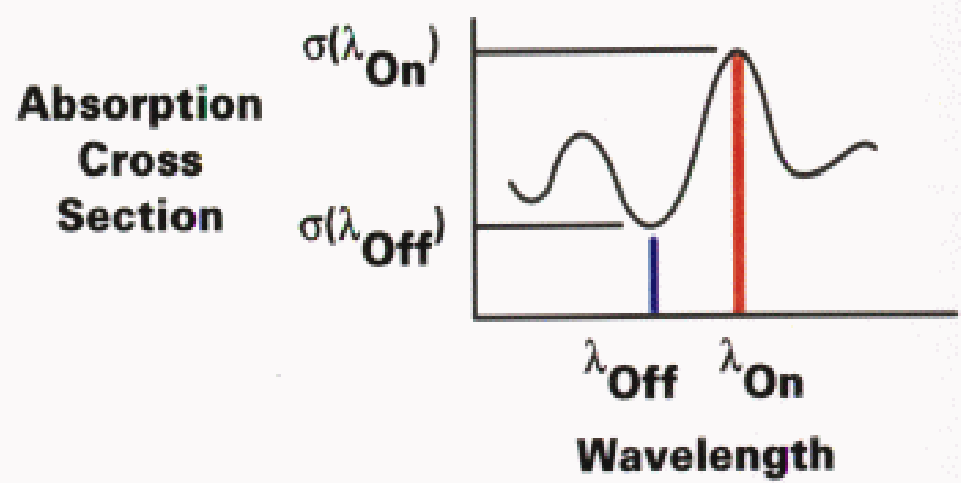
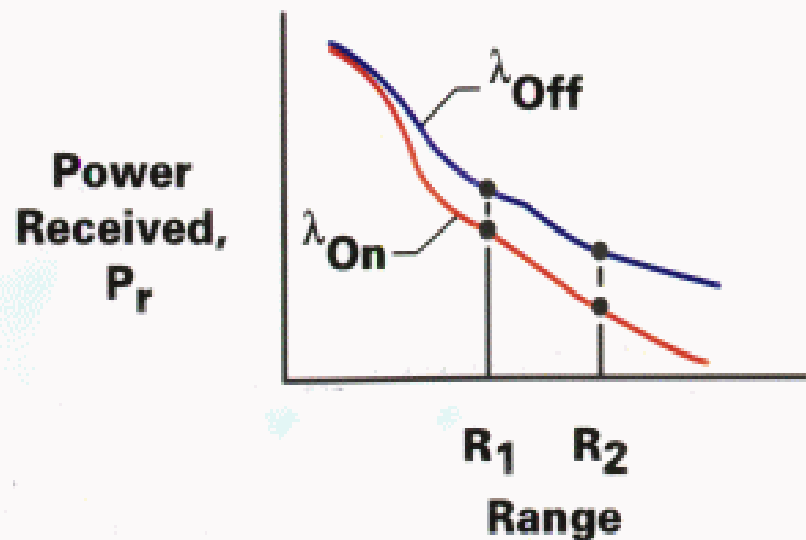
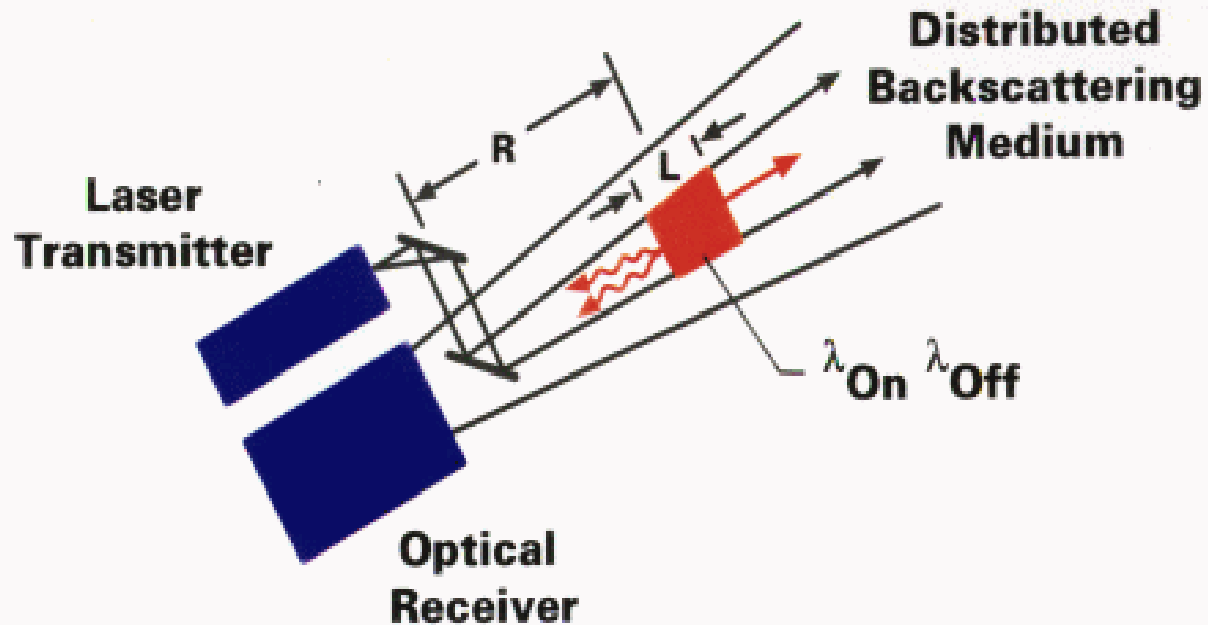
Guest lecture for ASEN-6519 Lidar Remote Sensing
CU Boulder

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Outline

- DIAL concept
- A short history of DIAL
- DIAL equation
- Precision & accuracy of DIAL retrieval
- Dual-DIAL technique

Differential Absorption Lidar (DIAL) Concept



Atmospheric gases measured with DIAL

- H_2O
- O_3
- SO_2
- NO_2 , NO
- NH_3
- CH_4
- CO_2
- Hg
- VOCs (Volatile Organic Compounds)
- Toluene, Benzene

First DIAL measurements

Richard M. Schotland (“The father of DIAL”)

1964 – Measured vertical profiles of water vapor by thermally tuning a ruby laser on and off the water vapor absorption line at 694.38 nm.

Only 4 years after invention of ruby laser !

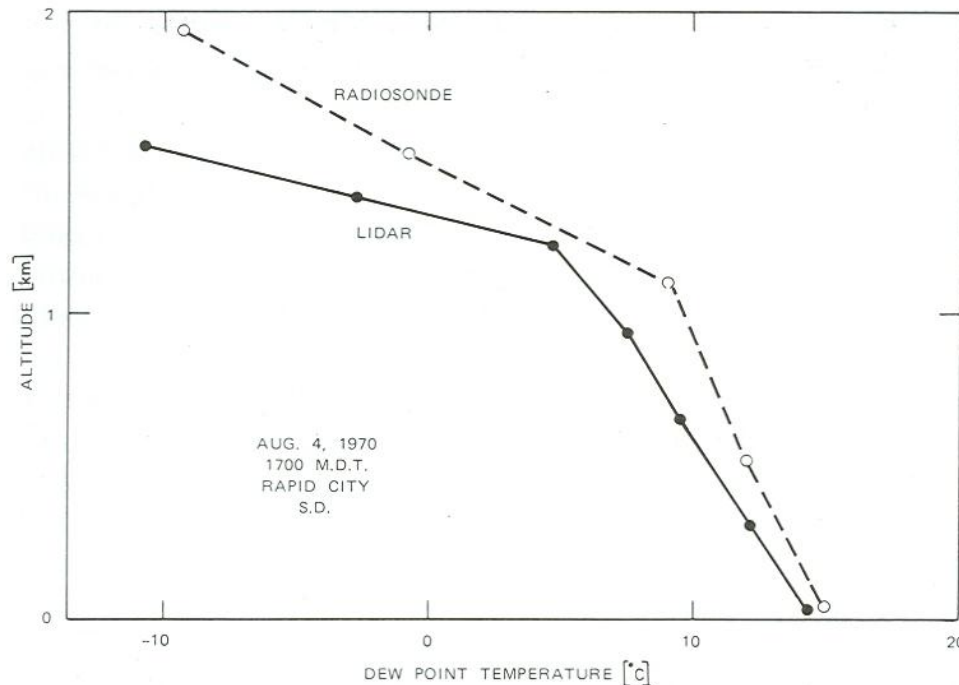
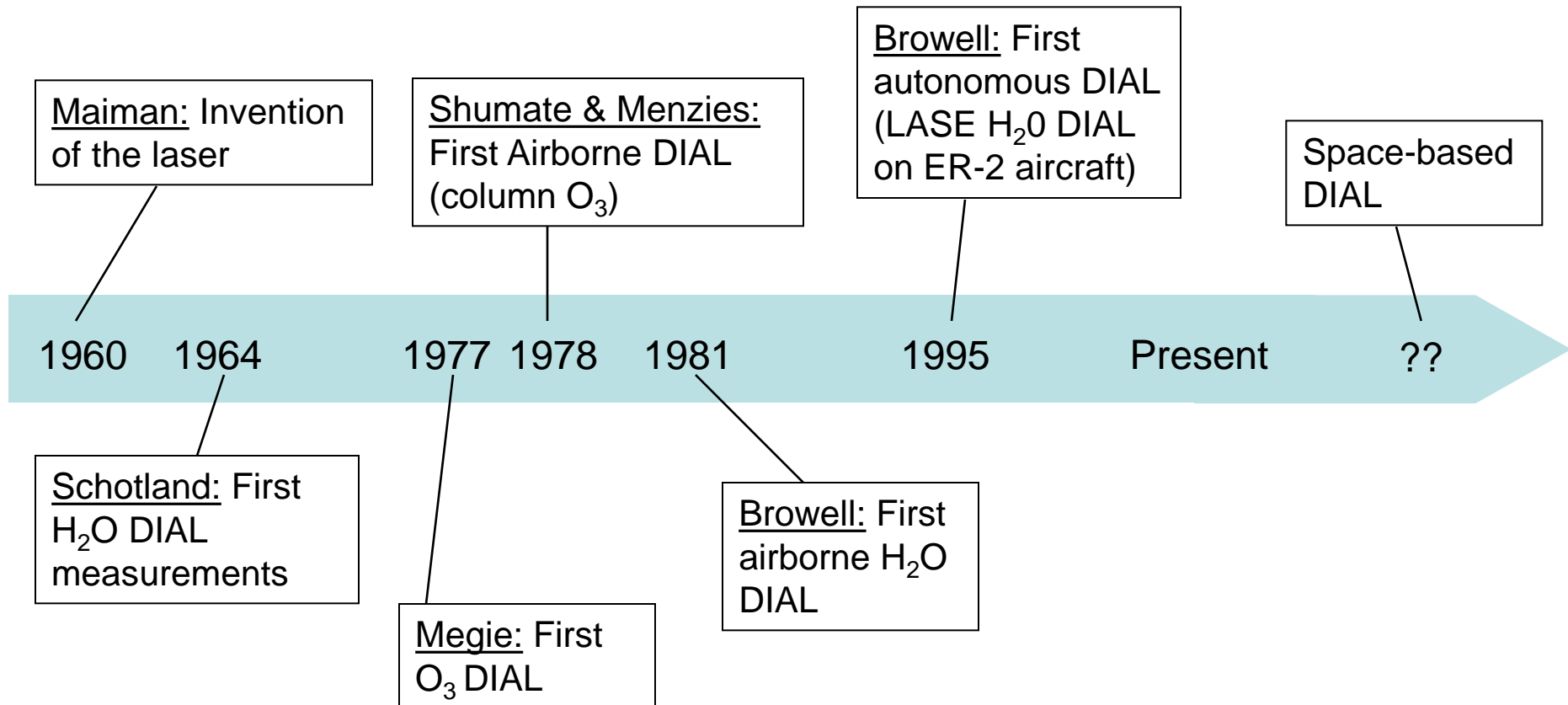


Fig. 4.20. Comparison of atmospheric water vapor vertical profiles (expressed as dew point temperature) measured by differential absorption lidar and radiosonde [4.82]

Major milestones in the history of DIAL



DIAL equation (1)

Single scattering, elastic backscatter LIDAR equation:

$$N_S(\lambda, R) = N_L(\lambda) [\beta(\lambda, R)\Delta R] \frac{A}{R^2} \exp\left[-2\int_0^R \alpha_{Tot}(\lambda, r) dr\right] [\eta(\lambda) G(\lambda, R)] + N_B(\lambda)$$

$$\text{with } \alpha_{Tot}(\lambda, r) = \alpha(\lambda, r) + \sum_i \sigma_{mol,abs,i}(\lambda, r) n_i(r)$$

Take ratio of LIDAR equations for online and offline wavelengths λ_{on} and λ_{off} :

$$\frac{N_S(\lambda_{off}, R) - N_B(\lambda_{off}, R)}{N_S(\lambda_{on}, R) - N_B(\lambda_{on}, R)} = \frac{N_L(\lambda_{off}) \eta(\lambda_{off}) G(\lambda_{off}, R) \beta(\lambda_{off}, R)}{N_L(\lambda_{on}) \eta(\lambda_{on}) G(\lambda_{on}, R) \beta(\lambda_{on}, R)} \\ \times \exp\left[-2\int_0^R \alpha(\lambda_{off}, r) - \alpha(\lambda_{on}, r) dr\right] \\ \times \exp\left[-2\int_0^R (\sigma_C(\lambda_{off}, r) - \sigma_C(\lambda_{on}, r)) n_C(r) dr\right] \\ \times \exp\left[-2\int_0^R \sum_{i=1}^m [(\sigma_{X_i}(\lambda_{off}, r) - \sigma_{X_i}(\lambda_{on}, r)) n_{X_i}(r)] dr\right]$$

**Number density
of constituent C**

DIAL equation (2)

$$n_c = \frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \left[\frac{N_S(\lambda_{off}, R) - N_B(\lambda_{off})}{N_S(\lambda_{on}, R) - N_B(\lambda_{on})} \right]$$

$$- \frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \frac{G(\lambda_{off}, R)}{G(\lambda_{on}, R)} \quad [G]$$

$$- \frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \frac{\beta(\lambda_{off}, R)}{\beta(\lambda_{on}, R)} \quad [B]$$

$$- \frac{1}{\Delta\sigma_c(R)} [\alpha(\lambda_{on}, R) - \alpha(\lambda_{off}, R)] \quad [E]$$

$$- \frac{1}{\Delta\sigma_c(R)} \sum_{i=1}^m \Delta\sigma_{X_i}(R) n_{X_i}(R) \quad [X]$$

with $\Delta\sigma_c(R) = \sigma_c(\lambda_{on}, R) - \sigma_c(\lambda_{off}, R)$

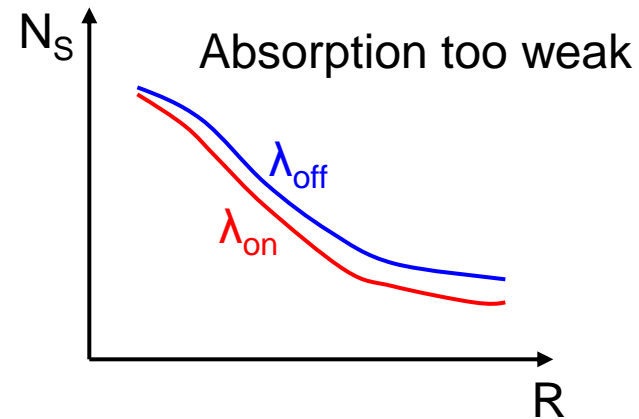
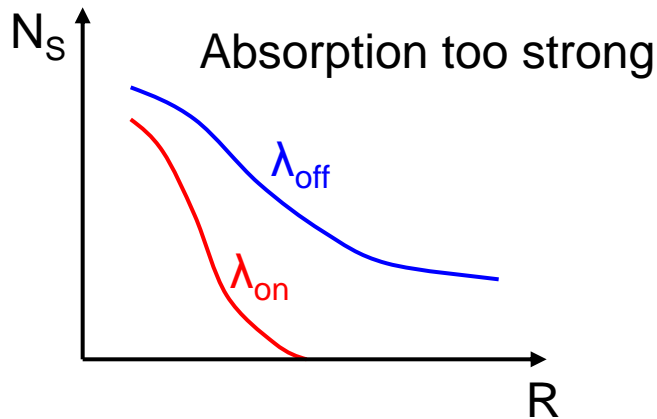
G = differential geometrical factor
E = differential extinction

B = differential backscatter
X = interfering constituents

How to choose an appropriate absorption line for DIAL (1)

$$N_s(\lambda_{on}, R) \propto \exp \left[-2 \int_0^R \sigma_C(\lambda_{on}, r) n_C(r) dr \right]$$

Extinction of online wavelength due to absorption by constituent C must be neither too small or too large.



Best precision in n_C when: $\tau(\lambda_{on}, R_{\max}) = \int_0^{R_{\max}} \sigma_C(\lambda_{on}, r) n_C(r) dr = 1.1$

(Remsberg & Gordley, 1978)

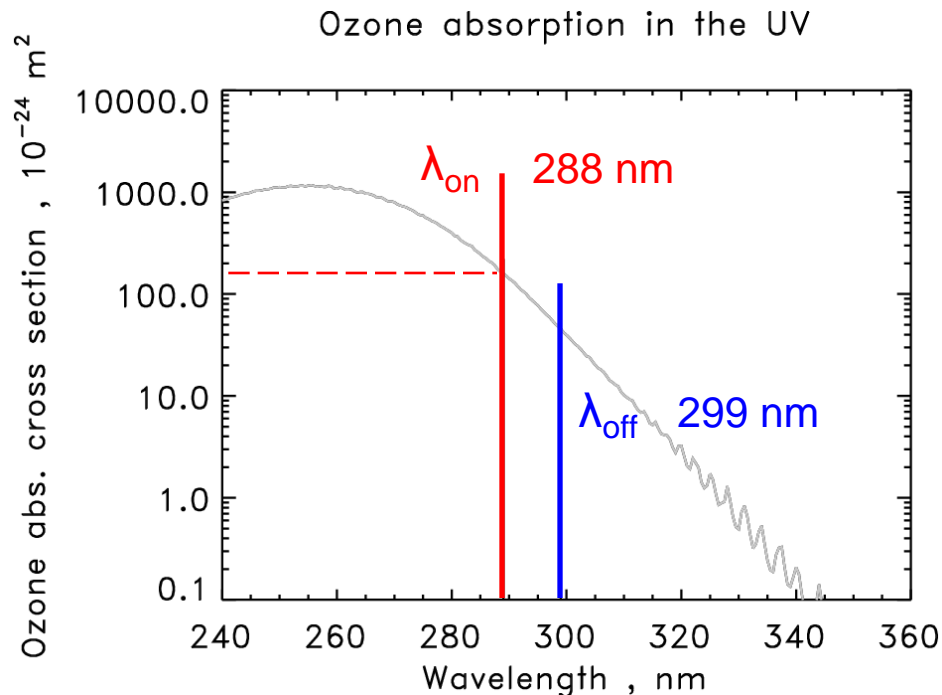
How to choose an appropriate absorption line for DIAL (2)

Example: Ozone

$$\tau(\lambda_{on}, R_{max}) = \int_0^{R_{max}} \sigma_C(\lambda_{on}, r) n_C(r) dr = 1.1$$

For $mr_{O_3} = 80 \text{ ppbv}$ or $n_{O_3} = 2 \times 10^{18} \text{ m}^{-3}$ and $R_{max} = 3 \text{ km}$:

$$\sigma_{O_3}(\lambda_{on}) n_{O_3} R_{max} = 1.1 \Rightarrow \sigma_{O_3}(\lambda_{on}) = 1.83 \times 10^{-22} \text{ m}^2$$



Precision of DIAL measurements

Simple “back of the envelope” calculation:

$$n_C = \frac{1}{2\Delta\sigma_C(R)\Delta R} \ln \left[\frac{N(\lambda_{off}, R + \Delta R) N(\lambda_{on}, R)}{N(\lambda_{on}, R + \Delta R) N(\lambda_{off}, R)} \right] \quad \text{with } N = N_S - N_B$$

$$\delta n_C = \frac{1}{2\Delta\sigma_C(R)\Delta R} \sqrt{\sum_{i,j} \frac{\delta^2(N(\lambda_i, R_j))}{(N(\lambda_i, R_j))^2}} \approx \frac{1}{\Delta\sigma_C \Delta R} \frac{\delta N}{N} = \frac{1}{\Delta\sigma_C \Delta R SNR} \quad \text{with } SNR = \frac{N}{\delta N}$$

$$\frac{\delta n_C}{n_C} = \frac{1}{\Delta\sigma_C n_C \Delta R SNR} = \frac{1}{\Delta\tau SNR} \Rightarrow \boxed{SNR = \frac{1}{\Delta\tau \delta n_C/n_C}}$$

$$\text{Example: } \Delta\tau = 0.05, \delta n_C/n_C = 5\% \Rightarrow \boxed{SNR = 400!}$$

Even modest precision of 5% requires high SNR. SNR can be increased by averaging on/offline signals time- and range-wise.

$$\text{Poisson statistics: } \delta N = N^{0.5} \Rightarrow SNR = N^{0.5}$$

$$\text{Since } N \propto \Delta t \Delta R, \quad \boxed{SNR \propto \Delta t^{0.5} \Delta R^{0.5} \quad \text{and} \quad \delta n_C \propto \Delta t^{-0.5} \Delta R^{-1.5}}$$

Accuracy of DIAL measurements (1)

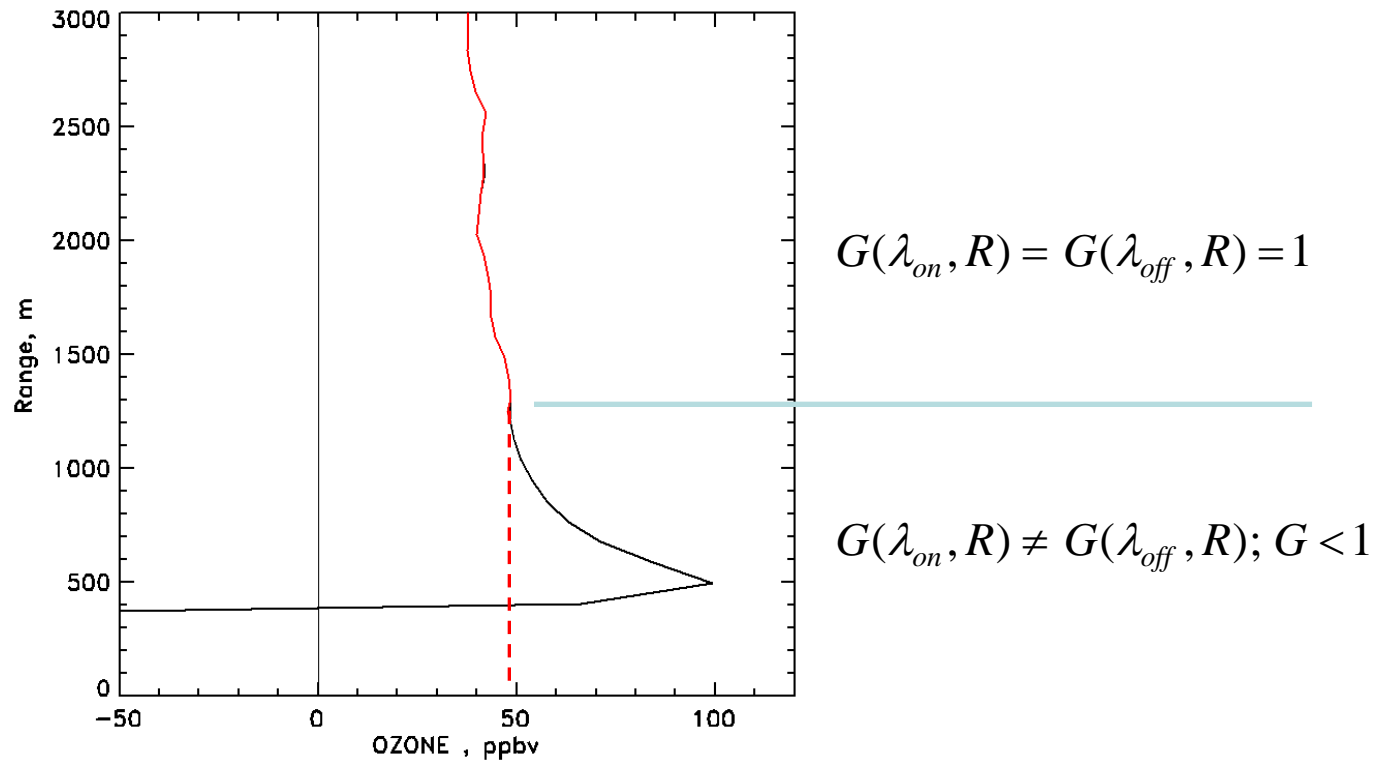
$$n_c = \frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \left[\frac{N_S(\lambda_{off}, R) - N_B(\lambda_{off})}{N_S(\lambda_{on}, R) - N_B(\lambda_{on})} \right]$$
$$- \frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \frac{G(\lambda_{off}, R)}{G(\lambda_{on}, R)} \quad [G]$$
$$- \frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \frac{\beta(\lambda_{off}, R)}{\beta(\lambda_{on}, R)} \quad [B]$$
$$- \frac{1}{\Delta\sigma_c(R)} [\alpha(\lambda_{on}, R) - \alpha(\lambda_{off}, R)] \quad [E]$$
$$- \frac{1}{\Delta\sigma_c(R)} \sum_{i=1}^m \Delta\sigma_{X_i}(R) n_{X_i}(R) \quad [X]$$

Accuracy affected by:

- How well is absorption cross section known?
- Improper correction of signal offsets, e.g. background light
- Geometrical factor different for λ_{on} and λ_{off}
- Differential backscatter & extinction not properly corrected
- Interfering species not taken into account

Accuracy of DIAL measurements (2)

Differential geometrical factor:
$$-\frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \frac{G(\lambda_{off}, R)}{G(\lambda_{on}, R)} \quad [G]$$



Effect of differential geometrical factor on O₃ retrieval

Accuracy of DIAL measurements (3)

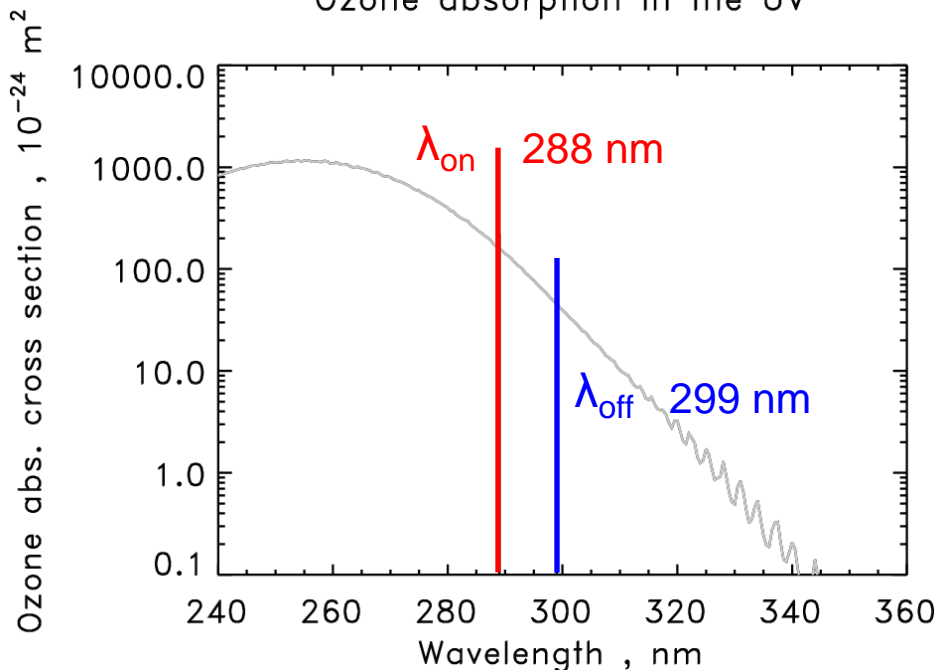
Differential backscatter & extinction:

$$-\frac{1}{2\Delta\sigma_c(R)} \frac{d}{dR} \ln \frac{\beta(\lambda_{off}, R)}{\beta(\lambda_{on}, R)} \quad [B]$$

$$-\frac{1}{\Delta\sigma_c(R)} [\alpha(\lambda_{on}, R) - \alpha(\lambda_{off}, R)] \quad [E]$$

$$\beta = \beta_{Rayleigh} + \beta_{Aerosol}, \quad \alpha = \alpha_{Rayleigh} + \alpha_{Aerosol}$$

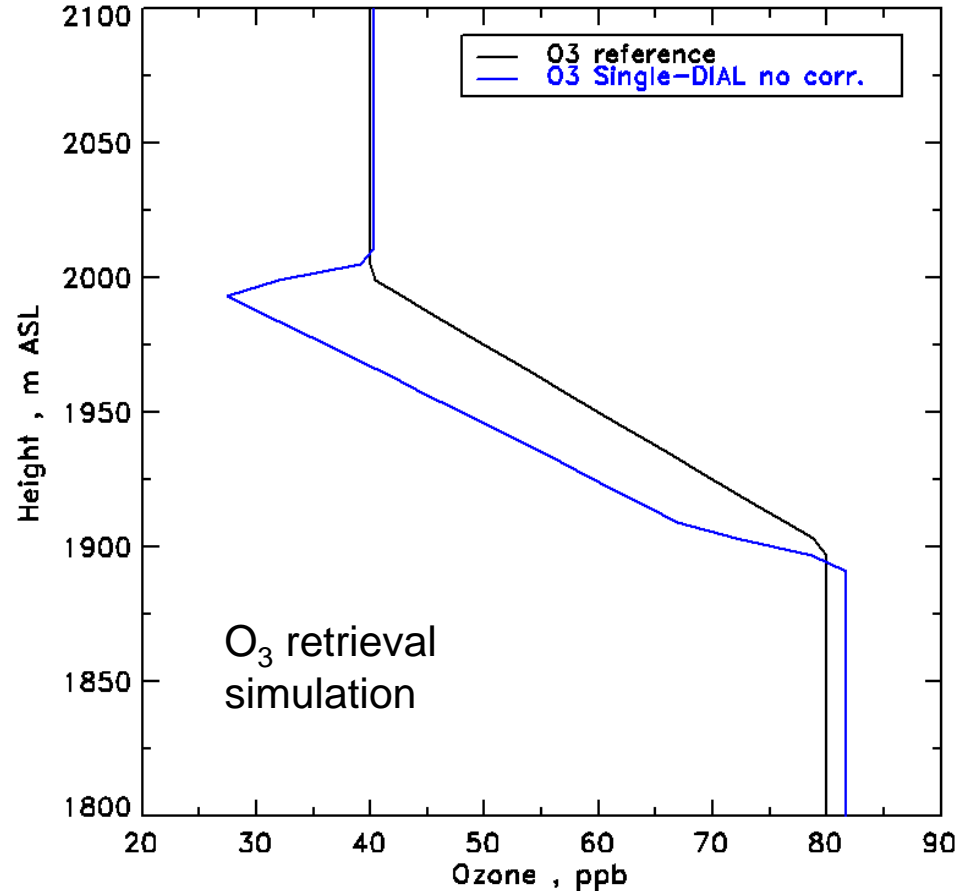
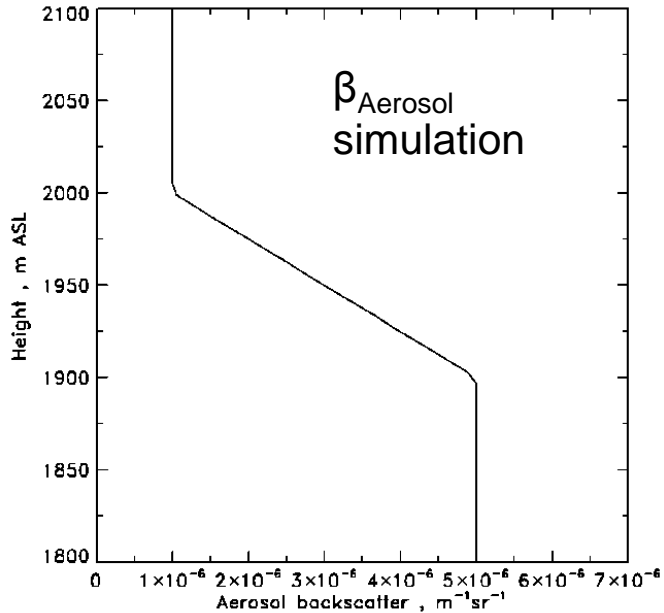
Ozone absorption in the UV



➤ For ozone DIAL retrieval, backscatter and extinction correction is necessary due to large $\Delta\lambda$.

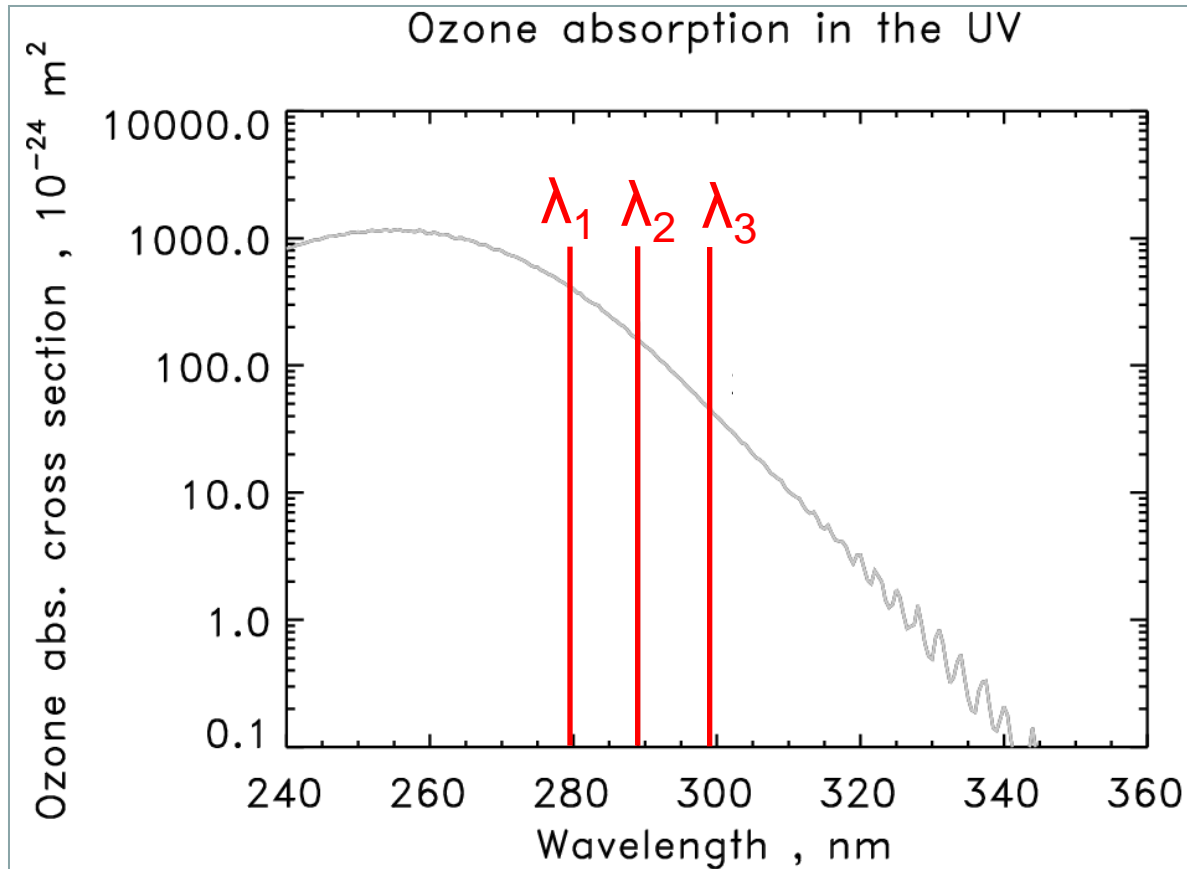
➤ $\beta_{Aerosol}$ and $\alpha_{Aerosol}$ have to be determined from offline signal data and wavelength dependence of β and α have to be guessed.

Accuracy of DIAL measurements (4)



Wrong assumptions about aerosol parameters can introduce significant errors in O₃ retrieval !

Dual-DIAL concept



2 DIAL wavelength pairs: λ_1 / λ_2 and λ_2 / λ_3

Dual-DIAL minimizes aerosol interference (1)

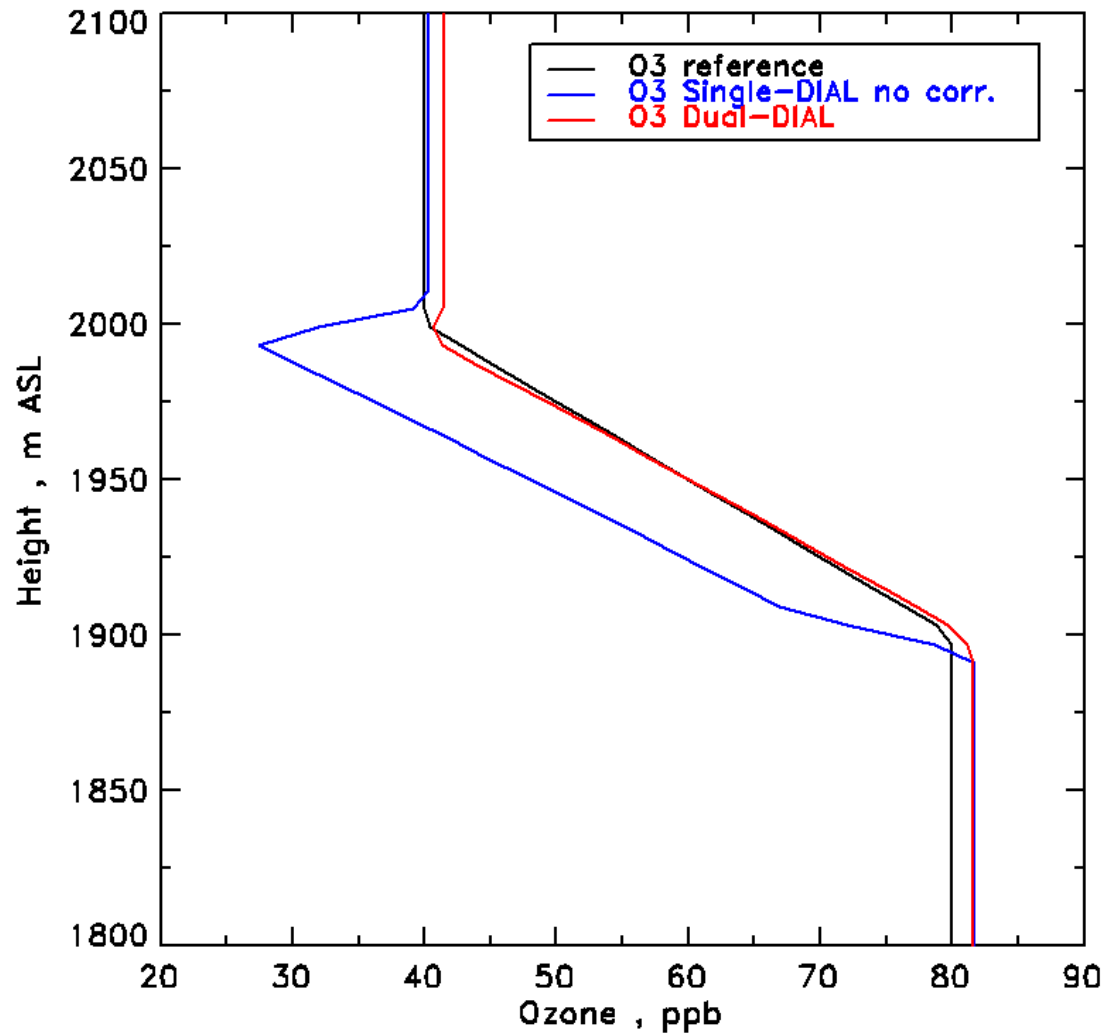
$$\begin{aligned}
 n_C = & \frac{1}{2 \delta \sigma_C(R)} \frac{d}{dR} \left[\ln \frac{N_S^*(\lambda_{off1}, R)}{N_S^*(\lambda_{on1}, R)} - C \ln \frac{N_S^*(\lambda_{off2}, R)}{N_S^*(\lambda_{on2}, R)} \right] \\
 & - \frac{1}{2 \delta \sigma_C(R)} \frac{d}{dR} \left[\ln \frac{\beta(\lambda_{off1}, R)}{\beta(\lambda_{on1}, R)} - C \ln \frac{\beta(\lambda_{off2}, R)}{\beta(\lambda_{on2}, R)} \right] \quad [B'] \\
 & - \frac{1}{\delta \sigma_C(R)} \left[\alpha(\lambda_{on1}, R) - \alpha(\lambda_{off1}, R) - C(\alpha(\lambda_{on2}, R) - \alpha(\lambda_{off2}, R)) \right] \quad [E']
 \end{aligned}$$

with $\delta \sigma_C(R) = \Delta \sigma_{C1} - C \Delta \sigma_{C2}$, DIAL pair 1: $\lambda_{on1} / \lambda_{off1}$, DIAL pair 2: $\lambda_{on2} / \lambda_{off2}$

$$B' = E' \approx 0 \quad \text{for} \quad C = \frac{\lambda_{on1} - \lambda_{off1}}{\lambda_{on2} - \lambda_{off2}}$$

- No correction of differential aerosol effects needed and residual errors are small.
- However, precision of DIAL retrieval is degraded.

Dual-DIAL minimizes aerosol interference (2)



O₃ retrieval simulation

Selected References

DIAL history (slides 5 - 6)

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How to choose a DIAL absorption line? (slides 9 - 10)

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Aerosol correction & DUAL-DIAL (slides 14 - 18)

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